



# Co-design of event generator and filtering for a class of T–S fuzzy systems with stochastic sensor faults

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## Abstract

This paper is firstly concerned with reliable  $H_\infty$  filter design for a class of T–S fuzzy systems with stochastic sensor faults under an event triggered scheme. 1) A T–S fuzzy model is used to approximate the nonlinear dynamics of the plant. A set of stochastic variables are used to describe the sensor failure. 2) An event-triggered scheme, which has some advantages over some existing ones, is introduced to the networked control systems. Under the event-triggered scheme, the sensor data are transmitted only when the sampled measurements of the plant violate the specified event condition. Then, an event-based filter design model for T–S fuzzy systems is constructed by taking the effect of event-triggered scheme and the sensor faults into consideration. Sufficient conditions for the existence of the desired filter are established in terms of linear matrix inequalities and the explicit expression is given for the designed filter parameters. A numerical example is provided to illustrate the design method.

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**Keywords:** Reliable filter design; Stochastic sensor failure; Event-triggered scheme; T–S fuzzy systems; Networked control systems

## 1. Introduction

The control problem for T–S fuzzy systems has received considerable attention in recent years. It has been proved that T–S fuzzy systems, which can be analyzed by many properties of conventional linear systems and described by a family of IF–THEN rules, can approximate any continuous functions [1–3]. Over the past few years, a great effort has been made on the stability analysis and synthesis for T–S fuzzy systems. More specifically, the filtering problems for T–S fuzzy systems have been widely investigated by many researchers via various methodologies [4–6]. In [4], a class of T–S fuzzy stochastic systems was investigated. In [5], the authors investigated the robust and reliable

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$H_\infty$  filter design for a class of nonlinear NCSs with random sensor faults via T–S fuzzy model. The authors in [6] investigated the  $H_\infty$  filtering issue for nonlinear systems with time delay via T–S fuzzy systems.

The insertion of network in the control systems has many advantages such as low cost, reduced weight and power requirements, simple installation and maintenance, and high reliability. However, it can also bring about new interesting and challenging issues as to the limited capacity of the network cable, for example, the transmission delay, packet dropout, etc. Recently, some work has been made to increase the energy efficiency and reduce the cost of sensor network. There has been many publications in the literature [7,8]. Most of the available results employ time-triggered communication scheme. However, this might lead to insufficient utilization of limited resource and communication bandwidth. Especially when the system is close to its equilibrium point, there is little new information to be transmitted, thus, redundant communications have inevitably occurred [9]. Therefore, it is necessary to build a communication mechanism in a unified framework. Recently, event-triggered method has received considerable attention, which can reduce the burden of the network communication and the occupation of the sensor. Many outstanding results under event-triggered method have been available [9–13]. For example, in [10], the authors proposed a novel event-triggered scheme and constructed a delay system model for the analysis, then they derived the criteria for stability with an  $H_\infty$  norm bound and criteria for co-designing both the feedback gain and the trigger parameters. The authors in [11] proposed another event-triggered communication scheme and investigated a reliable control design for networked control system under event-triggered scheme. Little attention has been paid to the filtering problem for T–S fuzzy systems under event-triggered scheme. However, in distributed industrial networked control systems, the sensors can be in a hostile environment and subject to failure and the capacity of the network cable is limited, which may lead to intolerable system performance. Therefore, it is necessary to introduce an event-triggering sampling mechanism, which takes the probabilistic sensor and actuator faults into consideration. One of the main focuses of this paper is to propose a fault-tolerant event-triggered scheme to reduce the computation load or to reduce the exchange of information between the control agents (sensors, controller, actuator), the advantage of the proposed event-triggering sampling mechanism is that it only needs a supervision of the system state in discrete instants, there is no need to retrofit the existing system. The implementation of our event-triggering sampling scheme only monitors the system state in discrete instants. Up to now, to the best of the authors’ knowledge, event-triggered filtering for a class of T–S fuzzy systems with stochastic sensor faults has not been well addressed. This situation has motivated our current investigation.

In this paper, we introduce an event-triggered communication scheme to save the limited network resources while preserving the desired performance. The scheme can decide whether or not the sampled sensor measurements are to be transmitted. Only when the current sampled sensor measurements violate a special condition, then they can be transmitted. The overall purpose of this paper is to investigate the reliable  $H_\infty$  filter design for a class of T–S fuzzy systems under event-triggered scheme. The main contributions of this paper are as follows: 1) a new kind of T–S fuzzy systems under event-triggered scheme with probabilistic sensor faults is proposed, which has not been considered in the existing references; 2) sufficient conditions are derived for the existence of the desired  $H_\infty$  filter in terms of linear matrix inequalities. Based on the derived conditions, the event generator and filtering can be co-designed.

The paper is organized as follows. Section 2 presents the formation of the event-based T–S fuzzy systems with stochastic sensor faults. In Section 3, a sufficient condition for the existence of the desired filter is established in terms of linear matrix inequalities (LMIs) and a filter design method is provided. A numerical example is employed in the final part to demonstrate the effectiveness and applicability of our method.

Notation:  $\mathbb{R}^n$  and  $\mathbb{R}^{n \times m}$  denote the  $n$ -dimensional Euclidean space, and the set of  $n \times m$  real matrices; the superscript “ $T$ ” stands for matrix transposition;  $I$  is the identity matrix of appropriate dimension;  $\| \cdot \|$  stands for the Euclidean vector norm or the induced matrix 2-norm as appropriate; the notation  $X > 0$  (respectively,  $X \geq 0$ ), for  $X \in \mathbb{R}^{n \times n}$  means that the matrix  $X$  is real symmetric positive definite (respectively, positive semi-definite). For a matrix  $B$  and two symmetric matrices  $A$  and  $C$ ,  $\begin{bmatrix} A & * \\ B & C \end{bmatrix}$  denotes a symmetric matrix, where  $*$  denotes the entries implied by symmetry.

## 2. System description

As is shown in Fig. 1, consider the following T–S fuzzy system with  $r$  plant rules

$$R^i : \text{IF } \theta_1(t) \text{ is } W_1^i \text{ and } \cdots \text{ and } \theta_g(t) \text{ is } W_g^i,$$

THEN

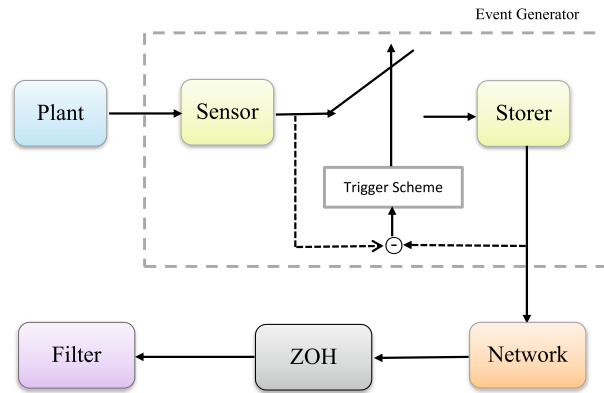


Fig. 1. The structure of an event-triggered filtering system.

$$\begin{cases} \dot{x}(t) = A_i x(t) + A_{di} x(t - \tau(t)) + A_{\omega i} \omega(t) \\ y(t) = C_i x(t) \\ z(t) = L_i x(t) \end{cases} \tag{1}$$

where  $i = 1, 2, \dots, r$ ,  $r$  is the number of IF–THEN rules,  $\theta_1(t), \theta_2(t), \dots, \theta_g(t)$  are the premise variables,  $x(t) \in \mathbb{R}^n$ ,  $y(t) \in \mathbb{R}^m$  and  $z(t) \in \mathbb{R}^p$  are the state vector, output vector and the signal to be estimated, respectively.  $A_i, A_{di}, A_{\omega i}, C_i, L_i, i \in \mathcal{S} = \{1, 2, \dots, r\}$ , are parameter matrices with appropriate dimensions,  $\omega(t) \in L_2[0, \infty)$  denotes the exogenous disturbance signal,  $\tau(t)$  is a time-varying delay taking values on the interval  $[\tau_m, \tau_M]$ , where  $\tau_m$  and  $\tau_M$  are positive real numbers.

By using center-average defuzzifier, product interference and singleton fuzzifier, the global dynamics of (1) can be inferred as

$$\begin{cases} \dot{x}(t) = A(t)x(t) + A_d(t)x(t - \tau(t)) + A_\omega(t)\omega(t) \\ y(t) = C(t)x(t) \\ z(t) = L(t)x(t) \end{cases} \tag{2}$$

where  $A(t) = \sum_{i=1}^r h_i A_i$ ,  $A_d(t) = \sum_{i=1}^r h_i A_{di}$ ,  $A_\omega(t) = \sum_{i=1}^r h_i A_{\omega i}$ ,  $C(t) = \sum_{i=1}^r h_i C_i$ ,  $L(t) = \sum_{i=1}^r h_i L_i$ .  $h_i$  is the abbreviation for  $h_i(\theta(t))$ ,  $h_i(\theta(t)) = \frac{\alpha_i(\theta(t))}{\sum_{i=1}^r \alpha_i(\theta(t))}$ ,  $\alpha_i(\theta(t)) = \prod_{j=1}^g W_j^i(\theta_j(t))$ ,  $W_j^i(\theta_j(t))$  is the grade membership value of  $\theta_j(t)$  in  $W_j^i$  and  $h_i(\theta(t))$  satisfies  $h_i(\theta(t)) \geq 0$ ,  $\sum_{i=1}^r h_i(\theta(t)) = 1$ .

The purpose of this paper is to design an  $H_\infty$  fuzzy filter, where  $i$ th rule is expressed in the following IF–THEN rule

$R^i$ : IF  $\theta_1(t)$  is  $W_1^i$  and  $\dots$  and  $\theta_g(t)$  is  $W_g^i$   
THEN

$$\begin{cases} \dot{x}_f(t) = A_{fi} x_f(t) + B_{fi} \hat{y}(t) \\ z_f(t) = C_{fi} x_f(t) \end{cases} \tag{3}$$

where  $i \in \mathcal{S} = \{1, 2, \dots, r\}$ .  $x_f(t) \in \mathbb{R}^n$ ,  $z_f(t) \in \mathbb{R}^p$  are the state and output of the filter, respectively.  $\hat{y}(t)$  is the real input of the filter. The matrices  $A_{fi} \in \mathbb{R}^{n \times n}$ ,  $B_{fi} \in \mathbb{R}^{n \times m}$ ,  $C_{fi} \in \mathbb{R}^{p \times n}$  are to be determined.

The defuzzified output of (3) is referred by

$$\begin{cases} \dot{x}_f(t) = A_f(t)x_f(t) + B_f(t)\hat{y}(t) \\ z_f(t) = C_f(t)x_f(t) \end{cases} \tag{4}$$

where  $A_f(t) = \sum_{i=1}^r h_i A_{fi}$ ,  $B_f(t) = \sum_{i=1}^r h_i B_{fi}$ ,  $C_f(t) = \sum_{i=1}^r h_i C_{fi}$ .

**Remark 1.** Under the traditional control system structure, the effect of the transmission delay can be neglected, that is  $\hat{y}(t) = y(t)$ . However, in networked control systems, the transmission delay should be take into account. In this paper, considering the existence of the network induced delay,  $\hat{y}(t) \neq y(t)$ .

Suppose the time-varying delay in the network communication is  $d_k$  and  $d_k \in [0, \bar{d}]$ , where  $\bar{d}$  is a positive real number. Therefore, the sampled sensor measurements  $y(t_0h), y(t_1h), y(t_2h), \dots$  will arrive at the filter side at the instants  $t_0h + d_0, t_1h + d_1, t_2h + d_2, \dots$ , respectively.  $\hat{y}(t)$  in Eq. (4) can be described as [5,14]

$$\hat{y}(t) = \sum_{i=1}^r h_i C_i x(t_k h), \quad t \in [t_k h + d_{t_k}, t_{k+1} h + d_{t_{k+1}}] \tag{5}$$

where  $h$  is the sampling period,  $t_k \in \{1, 2, 3, \dots\}$ .  $d_{t_k}$  and  $d_{t_{k+1}}$  are the network induced delays at the transmission instant  $t_k h$  and  $t_{k+1} h$ , respectively.

Considering the possible sensor failure, (5) can be rewritten as

$$\hat{y}(t) = \sum_{i=1}^r h_i \mathcal{E} C_i x(t_k h) = \sum_{i=1}^r \sum_{l=1}^m h_i \mathcal{E}_l E_l C_i x(t_k h), \quad t \in [t_k h + d_{t_k}, t_{k+1} h + d_{t_{k+1}}] \tag{6}$$

where  $\mathcal{E} = \text{diag}\{\mathcal{E}_1, \mathcal{E}_2, \dots, \mathcal{E}_m\}$  with  $\mathcal{E}_i (i = 1, 2, \dots, m)$  being  $m$  unrelated random variables taking values on the interval  $[0, \theta]$ ,  $\theta \geq 1$  and  $E_l = \text{diag}\{\underbrace{0, \dots, 0}_{l-1}, 1, \underbrace{0, \dots, 0}_{m-l}\}$ . The mathematical expectation and variance of  $\mathcal{E}_i$

( $i = 1, 2, \dots, m$ ) are  $\bar{\mathcal{E}}_i$  and  $\delta_i^2$ , respectively.  $\bar{\mathcal{E}}_i$  and  $\delta_i^2$  can be determined the failure rate and the distortion degree of the  $i$ th sensor.

Define  $\bar{\mathcal{E}} = \text{diag}\{\bar{\mathcal{E}}_1, \bar{\mathcal{E}}_2, \dots, \bar{\mathcal{E}}_m\}$ , we can easily derive  $\bar{\mathcal{E}} = \sum_{l=1}^m \bar{\mathcal{E}}_l E_l$ . For a matrix  $\Theta > 0$ , we can get

$$\begin{cases} \mathbb{E}\{\mathcal{E} - \bar{\mathcal{E}}\} = 0 \\ \mathbb{E}\{(\mathcal{E} - \bar{\mathcal{E}})^T \Theta (\mathcal{E} - \bar{\mathcal{E}})\} = \sum_{l=1}^m \delta_l^2 E_l^T \Theta E_l \end{cases}$$

**Remark 2.** When sensors have faults, the output signal may be larger or smaller than what it should be. Considering this case, we assume the variables  $\mathcal{E}_i (i = 1, 2, \dots, m)$  take values in the interval  $[0, \theta]$ ,  $\theta \geq 1$ . When  $\mathcal{E}_i \in \{0, 1\}$ , it means the sensor  $i$  has completely failure or not.  $\mathcal{E}_i = 1$  means the sensor  $i$  works normally,  $\mathcal{E}_i = 0$  means signal sent by sensor  $i$  is lost during transmission. Moreover,  $0 < \mathcal{E}_i < 1$  and  $\mathcal{E}_i > 1$  means the case of data distortion happen, that is, the signal at the filter is smaller or greater than it actually is.

As is well known, the widely used periodic sampling mechanism may lead to transmit many unnecessary signals, which reduces bandwidth utilization. In order to reduce the load of network transmission and save the network bandwidth, there is a great need to introduce an event triggered mechanism which decides whether the newly sampled data should be sent out to the filter. As is shown in Fig. 1, similar to [11], we introduce an event generator between the sensor and the filter. The sensor measurements are sampled regularly by the sampler of the smart sensor with period  $h$ , which will be given in sequel. Whether or not the newly sampled sensor measurements will be sent out to the filter are determined by the following judgment algorithm:

$$\begin{aligned} & [\mathbb{E}\{\bar{\mathcal{E}} y((k+j)h)\} - \mathbb{E}\{\bar{\mathcal{E}} y(kh)\}]^T \Omega [\mathbb{E}\{\bar{\mathcal{E}} y((k+j)h)\} - \mathbb{E}\{\bar{\mathcal{E}} y(kh)\}] \\ & \leq \rho [\mathbb{E}\{\bar{\mathcal{E}} y((k+j)h)\}]^T \Omega \mathbb{E}\{\bar{\mathcal{E}} y((k+j)h)\} \end{aligned} \tag{7}$$

where  $\Omega$  is a symmetric positive definite matrix,  $j = 1, 2, \dots$ , and  $\rho \in [0, 1)$ . Only when the current sampled sensor measurements  $y((k+j)h)$  and the latest transmitted sensor measurements  $y(kh)$  variate the specified threshold (7), the current sampled sensor measurements  $y((k+j)h)$  can be transmitted by the event generator and sent into the filter.

**Remark 3.** From event-triggered algorithm (7), it is easily seen that the sensor measurement are sampled at time  $kh$  by sampler with a given period  $h$ , the next sensor measurement is at time  $(k+1)h$ . Suppose that the release times are  $t_0h, t_1h, t_2h, \dots$ , it is easily seen that  $s_i h = t_{i+1} h - t_i h$  denotes the release period of event generator in (7),  $s_i h$  means that the sampling between the two conjoint transmitted instant.

**Remark 4.** It is easily seen from event-triggered algorithm (7) that the set of the release instants  $\{t_0h, t_1h, t_2h, \dots\} \subseteq \{0, 1, 2, \dots\}$ . The amount of  $\{t_0h, t_1h, t_2h, \dots\}$  depends on the value of  $\rho$  and the variation of the sensor measurements.

Similar to [10–12] for technical convenience, consider the following two cases:

*Case 1:* If  $t_kh + h + \bar{d} \geq t_{k+1}h + d_{k+1}$ , where  $\bar{d} = \max d_k$ , define a function  $d(t)$  as

$$d(t) = t - t_kh, \quad t \in [t_kh + d_k, t_{k+1}h + d_{k+1}) \tag{8}$$

It can easily be obtained that

$$d_k \leq d(t) \leq (t_{k+1} - t_k)h + d_{k+1} \leq h + \bar{d} \tag{9}$$

*Case 2:* If  $t_kh + h + \bar{d} < t_{k+1}h + d_{k+1}$ , consider the following two intervals:

$$[t_kh + d_k, t_kh + h + \bar{d}), \quad [t_kh + ih + \bar{d}, t_kh + ih + h + \bar{d})$$

Since  $d_k \leq \bar{d}$ , it can be easily shown that there exists a positive integer  $\delta_M \geq 1$  such that

$$t_kh + \delta_Mh + \bar{d} < t_{k+1}h + d_{k+1} \leq t_kh + \delta_Mh + h + \bar{d}$$

Moreover,  $x(t_kh)$  and  $t_kh + ih$  with  $i = 1, 2, \dots, \delta_M$  satisfy (7). Let

$$\begin{cases} I_0 = [t_kh + d_k, t_kh + h + \bar{d}) \\ I_i = [t_kh + ih + \bar{d}, t_kh + ih + h + \bar{d}) \\ I_{\delta_M} = [t_kh + \delta_Mh + \bar{d}, t_{k+1}h + d_{k+1}) \end{cases} \tag{10}$$

where  $i = 1, 2, \dots, \delta_M - 1$ . It can be easily shown that

$$[t_kh + d_k, t_{k+1}h + d_{k+1}) = \bigcup_{i=0}^{i=\delta_M} I_i \tag{11}$$

Define

$$d(t) = \begin{cases} t - t_kh, & t \in I_0 \\ t - t_kh - ih, & t \in I_i, i = 1, 2, \dots, \delta_M - 1 \\ t - t_kh - \delta_Mh, & t \in I_{\delta_M} \end{cases} \tag{12}$$

From the definition of  $d(t)$ , we have

$$\begin{cases} t_k \leq d(t) < h + \bar{d}, & t \in I_0 \\ t_k \leq \bar{d} \leq d(t) < h + \bar{d}, & t \in I_i, i = 1, 2, \dots, \delta_M - 1 \\ t_k \leq \bar{d} \leq d(t) < h + \bar{d}, & t \in I_{\delta_M} \end{cases} \tag{13}$$

where the third row in (10) holds because  $t_{k+1}h + d_{k+1} \leq t_kh + (\delta_M + 1)h + \bar{d}$ . Obviously,

$$0 \leq d_k \leq d(t) \leq h + \bar{d} \triangleq d_M, \quad t \in [t_kh + d_k, t_{k+1}h + d_{k+1}) \tag{14}$$

In Case 1, for  $t \in [t_kh + d_k, t_{k+1}h + d_{k+1})$ , define an error vector  $e_k(t) = 0$ . In Case 2, define the mathematical expectation of the sensor measurement error between the current sampling instant and the latest transmission instant

$$\bar{\Xi} e_k(t) = \begin{cases} 0, & t \in I_0 \\ \bar{\Xi} y(t_kh) - \bar{\Xi} y(t_kh + ih), & t \in I_i, i = 1, 2, \dots, \delta_M - 1 \\ \bar{\Xi} y(t_kh) - \bar{\Xi} y(t_kh + \delta_Mh), & t \in I_{\delta_M} \end{cases} \tag{15}$$

From the definition of  $\bar{\Xi} e_k(t)$  and the triggering algorithm (7), it can be easily seen that for  $t \in [t_kh + d_k, t_{k+1}h + d_{k+1})$

$$e_k^T(t) \bar{\Xi}^T \Omega \bar{\Xi} e_k(t) \leq \rho y^T(t - d(t)) \bar{\Xi}^T \Omega \bar{\Xi} y(t - d(t)) \tag{16}$$

Here, the measurement output is sampled before it enters the filter; based on the sampling technique and zero-order hold, the actual output can be described as

$$y(t_kh) = \sum_{i=1}^r h_i \Xi C_i x(t_kh) \tag{17}$$

**Remark 5.** Notice that the relation of  $t_k h + h + \bar{d} \geq t_{k+1} h + d_{k+1}$  in Case 1 means the newly sampled sensor measurement  $y(t_k h + h)$  will be transmitted and arrive at the filter side at the instant  $t_k h + h + d_{k+1}$ ;  $t_k h + h + \bar{d} < t_{k+1} h + d_{k+1}$  in Case 2 means the newly sampled sensor measurement  $y(t_k h + h)$  and the latest sensor measurement  $y(t_k h)$  variate the judgment algorithm (7), and  $y(t_k h + h)$  will not be transmitted to the filter side.

**Remark 6.** From (15), we can deduce that the sensor measurement error between the current sampling instant and the latest transmission instant can be calculated as

$$e_k(t) = \begin{cases} 0, & t \in I_0 \\ y(t_k h) - y(t_k h + ih), & t \in I_i, i = 1, 2, \dots, \delta_M - 1 \\ y(t_k h) - y(t_k h + \delta_M h), & t \in I_{\delta_M} \end{cases} \quad (18)$$

**Remark 7.** It is seen from the definition of  $d(t)$  that  $d(t)$  is different from the traditional time-varying delay.  $d(t)$  depends not only on the release times, but also on the network induce delay  $d_k$  and the sampling period  $h$ .

**Remark 8.** Since there is a communication network between the sensor and the filter, the premises in the system and the ones in the filter should be asynchronous. That is, at the same instant  $t \in [t_k h + d_k, t_{k+1} h + d_{k+1})$ , when  $\theta_i(t)$  is available in (2), only  $\theta_i(t_k h)$  is available in the filter. In this paper, we assume the mechanical model of the studied system is known a priori, when the initial condition is given and the state of the studied system can be calculated based on the known mechanical model. Since  $\theta_i(t_k h)$  is available at the filter,  $\theta_i(t)$  can be calculated for  $t \in [t_k h, t_{k+1} h)$ . Therefore, the synchronous premise variables  $\theta_i(t)$  can be derived in the filter side.

Based on the above description, combining (17) and (13), from (6) and (15), the filter input can be rewritten as

$$\hat{y}(t) = \sum_{i=1}^r h_i \bar{\mathcal{E}} C_i x(t - d(t)) + \bar{\mathcal{E}} e_k(t) + \sum_{i=1}^r h_i ((\mathcal{E} - \bar{\mathcal{E}}) C_i x(t - d(t))), \quad t \in [t_k h + d_k, t_{k+1} h + d_{k+1}) \quad (19)$$

Combining (4) and (19), the defuzzified value of the filter can be rewritten as

$$\begin{cases} \dot{x}_f(t) = \sum_{i=1}^r \sum_{j=1}^r h_i h_j (A_{fi} x_f(t) + B_{fi} (\bar{\mathcal{E}} C_i x(t - d(t)) + \bar{\mathcal{E}} e_k(t) + (\mathcal{E} - \bar{\mathcal{E}}) C_i x(t - d(t)))) \\ z_f(t) = \sum_{i=1}^r \sum_{j=1}^r h_i h_j C_{fij} x_f(t) \end{cases} \quad (20)$$

Define  $e(t) = \begin{bmatrix} x(t) \\ x_f(t) \end{bmatrix}$ ,  $\tilde{z}(t) = z(t) - z_f(t)$ , the following filtering-error system based on Eqs. (2) and (20) can be obtained as

$$\begin{cases} \dot{e}(t) = \sum_{i=1}^r \sum_{j=1}^r h_i h_j \{ \bar{A} e(t) + \bar{A}_d H e(t - \tau(t)) + \bar{B} H e(t - d(t)) + \bar{B}_1 e_k(t) + \bar{A}_w w(t) + \bar{B}_i H e(t - d(t)) \} \\ \tilde{z}(t) = \sum_{i=1}^r \sum_{j=1}^r h_i h_j \bar{L} e(t) \end{cases} \quad (21)$$

where

$$\begin{aligned} \bar{A} &= \begin{bmatrix} A_i & 0 \\ 0 & A_{fj} \end{bmatrix}, & \bar{A}_d &= \begin{bmatrix} A_{di} \\ 0 \end{bmatrix}, & \bar{B} &= \begin{bmatrix} 0 \\ B_{fj} \bar{\mathcal{E}} C_i \end{bmatrix}, & \bar{B}_1 &= \begin{bmatrix} 0 \\ B_{fj} \bar{\mathcal{E}} \end{bmatrix}, & \bar{A}_w &= \begin{bmatrix} A_{wi} \\ 0 \end{bmatrix}, \\ \bar{B}_i &= \begin{bmatrix} 0 \\ B_{fj} (\mathcal{E} - \bar{\mathcal{E}}) C_i \end{bmatrix}, & \bar{L} &= [L_i \quad -C_{fj}], & H &= [I \quad 0] \end{aligned}$$

**Remark 9.** When formulating the system (21), both of the transmission delay and event triggering condition (7) are taken into consideration. If  $\rho = 0$ , the event-triggered scheme reduces to a periodic release scheme, which implying that  $\bar{\mathcal{E}} e_k(t) = 0$ , then the sensor measurement degenerates into (6) and the system reduces to the case in [5], where

the robust and reliable filter design for T–S fuzzy model-based networked control systems with random sensor failure are studied.

In the following, we need to introduce two lemmas, which will help us in deriving the main results.

**Definition 1.** (See [15].) For a given function  $V : C_{F_0}^b([-\tau_M, 0], \mathbb{R}^n) \times S$ , its infinitesimal operator  $\mathcal{L}$  is defined as

$$\mathcal{L}(V\eta(t)) = \lim_{\Delta \rightarrow 0^+} \frac{1}{\Delta} [\mathbb{E}(V(\eta_t + \Delta) | \eta_t) - V(\eta_t)] \tag{22}$$

**Lemma 1.** (See [16].) For any vectors  $x, y \in \mathbb{R}^n$ , and positive definite matrix  $Q \in \mathbb{R}^{n \times n}$ , the following inequality holds:

$$2x^T y \leq x^T Q x + y^T Q^{-1} y$$

**Lemma 2.** (See [17].) Suppose  $\tau(t) \in [\tau_m, \tau_M]$ ,  $d(t) \in [0, d_M]$ ,  $\mathcal{E}_1, \mathcal{E}_2, \mathcal{E}_3, \mathcal{E}_4$  and  $\Omega$  are matrices with appropriate dimensions, then

$$(\tau(t) - \tau_m)\mathcal{E}_1 + (\tau_M - \tau(t))\mathcal{E}_2 + d(t)\mathcal{E}_3 + (d_M - d(t))\mathcal{E}_4 + \Omega < 0 \tag{23}$$

if and only if

$$\begin{aligned} (\tau_M - \tau_m)\mathcal{E}_1 + d_M\mathcal{E}_3 + \Omega &< 0 \\ (\tau_M - \tau_m)\mathcal{E}_2 + d_M\mathcal{E}_3 + \Omega &< 0 \\ (\tau_M - \tau_m)\mathcal{E}_1 + d_M\mathcal{E}_4 + \Omega &< 0 \\ (\tau_M - \tau_m)\mathcal{E}_2 + d_M\mathcal{E}_4 + \Omega &< 0 \end{aligned}$$

### 3. Main results

In this section, with a given filter with form (20), we will first propose the following performance analysis for the augmented systems (21). Then we deal with the design problem of the filter design for system (2).

**Theorem 1.** For given parameters  $\gamma, \tau_m, \tau_M, d_M$  and  $\rho$ , system (21) is exponentially stable in the mean square with an  $H_\infty$  disturbance attenuation level  $\gamma$  under the event trigger scheme (7) if there exist matrices  $P > 0, Q_k > 0, R_k > 0$  ( $k = 1, 2, 3$ ),  $\Omega > 0$ , and  $M_{ij}, N_{ij}, T_{ij}, S_{ij}$  with appropriate dimensions satisfying

$$\mathcal{E}^{ij} + \mathcal{E}^{ji} < 0, \quad i \leq j \in S \tag{24}$$

where

$$\begin{aligned} \mathcal{E}^{ij} &= \begin{bmatrix} \Omega_{11}^{ij} & * & * & * \\ \Omega_{21}^{ij} & \Omega_{22}^{ij} & * & * \\ \Omega_{31}^{ij} & 0 & \Omega_{33}^{ij} & * \\ \Omega_{41}^{ij}(s) & 0 & 0 & \Omega_{44}^{ij} \end{bmatrix}, \quad (s = 1, 2, 3, 4) \\ \Omega_{11}^{ij} &= \begin{bmatrix} \Gamma_{ij1} & * & * & * & * & * & * & * & * & * \\ R_2 & \Gamma_{ij2} & * & * & * & * & * & * & * & * \\ H^T \bar{A}_d^T P & M_{ij3} - M_{ij2}^T & \Gamma_{ij3} & * & * & * & * & * & * & * \\ 0 & 0 & N_{ij4} - N_{ij3}^T & \Gamma_{ij4} & * & * & * & * & * & * \\ H^T \bar{B}^T P + T_{ij5} - T_{ij1}^T & 0 & 0 & 0 & \Gamma_{ij5} & * & * & * & * & * \\ 0 & 0 & 0 & 0 & S_{ij6} - S_{ij5}^T & \Gamma_{ij6} & * & * & * & * \\ \bar{B}_1^T P & 0 & 0 & 0 & 0 & 0 & -\bar{\mathcal{E}}^T \Omega \bar{\mathcal{E}} & * & * & * \\ \bar{A}_w^T P & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -\gamma^2 I & * \end{bmatrix} \end{aligned}$$

$$\begin{aligned}
 \Gamma_{ij1} &= P\bar{A} + \bar{A}^T P + Q_1 + Q_2 + Q_3 - R_2 + T_{ij1} + T_{ij1}^T, & \Gamma_{ij2} &= -Q_1 - R_2 + M_{ij2} + M_{ij2}^T \\
 \Gamma_{ij3} &= -M_{ij3} - M_{ij3}^T + N_{ij3} + N_{ij3}^T, & \Gamma_{ij4} &= -Q_2 - N_{ij4} - N_{ij4}^T \\
 \Gamma_{ij5} &= \rho H^T C_i^T \bar{E}^T \Omega \bar{E} C_i H - T_{ij5} - T_{ij5}^T + S_{ij5} + S_{ij5}^T, & \Gamma_{ij6} &= -Q_3 - S_{ij6} - S_{ij6}^T \\
 \Omega_{21}^{ij} &= \begin{bmatrix} \bar{L} & 0 & 0 & 0 & 0 & 0 & 0 \\ \sqrt{\tau_{21}} P \bar{A} & 0 & \sqrt{\tau_{21}} P \bar{A}_d H & 0 & \sqrt{\tau_{21}} P \bar{B} H & 0 & \sqrt{\tau_{21}} P \bar{B}_1 & \sqrt{\tau_{21}} P \bar{A}_w \\ \tau_m P \bar{A} & 0 & \tau_m P \bar{A}_d H & 0 & \tau_m P \bar{B} H & 0 & \tau_m P \bar{B}_1 & \tau_m P \bar{A}_w \\ \sqrt{d_M} P \bar{A} & 0 & \sqrt{d_M} P \bar{A}_d H & 0 & \sqrt{d_M} P \bar{B} H & 0 & \sqrt{d_M} P \bar{B}_1 & \sqrt{d_M} P \bar{A}_w \end{bmatrix} \\
 \Omega_{22}^{ij} &= \text{diag}\{-I, -PR_1^{-1}P, -PR_2^{-1}P, -PR_3^{-1}P\}, & \Omega_{33}^{ij} &= \text{diag}\{\mathfrak{R}_1, \mathfrak{R}_2, \mathfrak{R}_3\}, \\
 \mathfrak{R}_k &= \text{diag}\{\underbrace{-PR_k^{-1}P, \dots, -PR_k^{-1}P}_m\}, & k &= 1, 2, 3, & \Omega_{44}^{ij} &= \text{diag}\{-R_1, -R_3\}, & \sqrt{\tau_{21}} &= \sqrt{\tau_M - \tau_m} \\
 \Omega_{31}^{ij} &= \begin{bmatrix} 0 & 0 & 0 & 0 & \check{D}_1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & \check{D}_2 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & \check{D}_3 & 0 & 0 & 0 \end{bmatrix}, & \check{D}_1 &= \begin{bmatrix} \sqrt{\tau_{21}} \delta_1 P \hat{D}_1 H \\ \vdots \\ \sqrt{\tau_{21}} \delta_m P \hat{D}_m H \end{bmatrix}, \\
 \check{D}_2 &= \begin{bmatrix} \delta_1 \tau_m P \hat{D}_1 H \\ \vdots \\ \delta_1 \tau_m \delta_m P \hat{D}_m H \end{bmatrix}, & \check{D}_3 &= \begin{bmatrix} \sqrt{d_M} \delta_1 P \hat{D}_1 H \\ \vdots \\ \sqrt{d_M} \delta_m P \hat{D}_m H \end{bmatrix}, & \hat{D}_l &= \begin{bmatrix} 0 \\ B_{fj} E_l C_i \end{bmatrix}, & l &= 1, 2, \dots, m \\
 \Omega_{41}^{ij}(1) &= \begin{bmatrix} \sqrt{\tau_{21}} M_{ij}^T \\ \sqrt{d_M} T_{ij}^T \end{bmatrix}, & \Omega_{41}^{ij}(2) &= \begin{bmatrix} \sqrt{\tau_{21}} M_{ij}^T \\ \sqrt{d_M} S_{ij}^T \end{bmatrix}, & \Omega_{41}^{ij}(3) &= \begin{bmatrix} \sqrt{\tau_{21}} N_{ij}^T \\ \sqrt{d_M} S_{ij}^T \end{bmatrix}, & \Omega_{41}^{ij}(4) &= \begin{bmatrix} \sqrt{\tau_{21}} N_{ij}^T \\ \sqrt{d_M} T_{ij}^T \end{bmatrix} \\
 M_{ij}^T &= [0 \quad M_{ij2}^T \quad M_{ij3}^T \quad 0 \quad 0 \quad 0 \quad 0 \quad 0], & N_{ij}^T &= [0 \quad 0 \quad N_{ij3}^T \quad N_{ij4}^T \quad 0 \quad 0 \quad 0 \quad 0] \\
 T_{ij}^T &= [T_{ij1}^T \quad 0 \quad 0 \quad 0 \quad T_{ij5}^T \quad 0 \quad 0 \quad 0], & S_{ij}^T &= [0 \quad 0 \quad 0 \quad 0 \quad S_{ij5}^T \quad S_{ij6}^T \quad 0 \quad 0]
 \end{aligned}$$

**Proof.** Choose the following Lyapunov functional candidate as

$$V(t) = V_1(t) + V_2(t) + V_3(t) \tag{25}$$

where

$$\begin{aligned}
 V_1(t) &= e^T(t) P e(t) \\
 V_2(t) &= \int_{t-\tau_m}^t e^T(s) Q_1 e(s) ds + \int_{t-\tau_M}^t e^T(s) Q_2 e(s) ds + \int_{t-d_M}^t e^T(s) Q_3 e(s) ds \\
 V_3(t) &= \int_{t-\tau_m}^{t-\tau_m} \int_s^t \dot{e}^T(v) R_1 \dot{e}(v) dv ds + \tau_m \int_{t-\tau_m}^t \int_s^t \dot{e}^T(v) R_2 \dot{e}(v) dv ds + \int_{t-d_M}^t \int_s^t \dot{e}^T(v) R_3 \dot{e}(v) dv ds
 \end{aligned}$$

and  $P > 0, Q_k > 0, R_k > 0 (k = 1, 2, 3)$ .

By applying the infinitesimal operator (Eq. (22)) for  $V_i(t) (i = 1, 2, 3)$  and taking expectation on it, we can obtain

$$\mathbb{E}\{\mathcal{L}V_1(t)\} = \sum_{i=1}^r \sum_{j=1}^r h_i h_j 2e^T(t) P \mathcal{A} \tag{26}$$

$$\begin{aligned}
 \mathbb{E}\{\mathcal{L}V_2(t)\} &= e^T(t) (Q_1 + Q_2 + Q_3) e(t) - e^T(t - \tau_m) Q_1 e(t - \tau_m) - e^T(t - \tau_M) Q_2 e(t - \tau_M) \\
 &\quad - e^T(t - d_M) Q_3 e(t - d_M)
 \end{aligned} \tag{27}$$



$$\begin{aligned} \mathbb{E}\{\mathcal{L}V_3(t)\} &= \sum_{i=1}^r \sum_{j=1}^r h_i h_j [\dot{e}^T(t) \tilde{R} \dot{e}(t)] - \int_{t-\tau_M}^{t-\tau_m} \dot{e}^T(s) R_1 \dot{e}(s) ds - \tau_m \int_{t-\tau_m}^t \dot{e}^T(s) R_2 \dot{e}(s) ds \\ &\quad - \int_{t-d_M}^t \dot{e}^T(s) R_3 \dot{e}(s) ds \end{aligned} \tag{28}$$

where  $\mathcal{A} = \bar{A}e(t) + \bar{A}_d H e(t - \tau(t)) + \bar{B} H e(t - d(t)) + \bar{B}_1 e_k(t) + \bar{A}_w w(t)$ ,  $\tilde{R} = (\tau_M - \tau_m) R_1 + \tau_m^2 R_2 + d_M R_3$ , and  $P > 0, Q_i > 0, R_i > 0 (i = 1, 2, 3)$

Notice that

$$-\tau_m \int_{t-\tau_m}^t \dot{e}^T(s) R_2 \dot{e}(s) ds \leq \begin{bmatrix} e(t) \\ e(t - \tau_m) \end{bmatrix}^T \begin{bmatrix} -R_2 & R_2 \\ R_2 & -R_2 \end{bmatrix} \begin{bmatrix} e(t) \\ e(t - \tau_m) \end{bmatrix} \tag{29}$$

Employing the free-weighting matrices method [18,19], it is easily derived that

$$2 \sum_{i=1}^r \sum_{j=1}^r h_i h_j \zeta^T(t) M_{ij} \left[ e(t - \tau_m) - e(t - \tau(t)) - \int_{t-\tau(t)}^{t-\tau_m} \dot{e}(s) ds \right] = 0 \tag{30}$$

$$2 \sum_{i=1}^r \sum_{j=1}^r h_i h_j \zeta^T(t) N_{ij} \left[ e(t - \tau(t)) - e(t - \tau_M) - \int_{t-\tau_M}^{t-\tau(t)} \dot{e}(s) ds \right] = 0 \tag{31}$$

$$2 \sum_{i=1}^r \sum_{j=1}^r h_i h_j \zeta^T(t) T_{ij} \left[ e(t) - e(t - d(t)) - \int_{t-d(t)}^t \dot{e}(s) ds \right] = 0 \tag{32}$$

$$2 \sum_{i=1}^r \sum_{j=1}^r h_i h_j \zeta^T(t) S_{ij} \left[ e(t - d(t)) - e(t - d_M) - \int_{t-d_M}^{t-d(t)} \dot{e}(s) ds \right] = 0 \tag{33}$$

where  $N_{ij}, M_{ij}, T_{ij}$  and  $S_{ij}$  are matrices with appropriate dimensions, and

$$\zeta^T(t) = [e^T(t) \quad e^T(t - \tau_m) \quad e^T(t - \tau(t)) \quad e^T(t - \tau_M) \quad e^T(t - d(t)) \quad e^T(t - d_M) \quad e_k^T(t) \quad w^T(t)]^T$$

By Lemma 1, we have

$$-2\zeta^T(t) M_{ij} \int_{t-\tau(t)}^{t-\tau_m} \dot{e}(s) ds \leq (\tau(t) - \tau_m) \zeta^T(t) M_{ij} R_1^{-1} M_{ij}^T \zeta(t) + \int_{t-\tau(t)}^{t-\tau_m} \dot{e}^T(s) R_1 \dot{e}(s) ds \tag{34}$$

$$-2\zeta^T(t) N_{ij} \int_{t-\tau_M}^{t-\tau(t)} \dot{e}(s) ds \leq (\tau_M - \tau(t)) \zeta^T(t) N_{ij} R_1^{-1} N_{ij}^T \zeta(t) + \int_{t-\tau_M}^{t-\tau(t)} \dot{e}^T(s) R_1 \dot{e}(s) ds \tag{35}$$

$$-2\zeta^T(t) T_{ij} \int_{t-d(t)}^t \dot{e}(s) ds \leq d(t) \zeta^T(t) T_{ij} R_3^{-1} T_{ij}^T \zeta(t) + \int_{t-d(t)}^t \dot{e}^T(s) R_3 \dot{e}(s) ds \tag{36}$$

$$-2\zeta^T(t) S_{ij} \int_{t-d_M}^{t-d(t)} \dot{e}(s) ds \leq (d_M - d(t)) \zeta^T(t) S_{ij} R_3^{-1} S_{ij}^T \zeta(t) + \int_{t-d_M}^{t-d(t)} \dot{e}^T(s) R_3 \dot{e}(s) ds \tag{37}$$

It is easy to obtain that

$$\begin{aligned} & \mathbb{E}\{\dot{e}^T(t)\tilde{R}\dot{e}(t)\} \\ &= \sum_{i=1}^r \sum_{j=1}^r h_i h_j \left\{ \mathcal{A}^T \tilde{R} \mathcal{A} + \sum_{l=1}^m \delta_l^2 e^T(t-d(t)) H^T \hat{D}_l^T \tilde{R} \hat{D}_l H e^T(t-d(t)) \right\} \end{aligned} \tag{38}$$

Combining (16) and (25)–(38), we can obtain that

$$\begin{aligned} & \mathbb{E}\{\mathcal{L}V(t) - \gamma^2 w^T(t)w(t) + \tilde{z}^T(k)\tilde{z}(k)\} \\ & \leq \sum_{i=1}^r \sum_{j=1}^r h_i h_j \{ \zeta^T(t) \Omega_{11}^{ij} \zeta(t) + \mathcal{A}^T H^T \tilde{R} H \mathcal{A} + e^T(t) \bar{L}^T \bar{L} e(t) \\ & \quad + \rho e^T(t-d(t)) H^T C_i^T \bar{E}^T \Omega \bar{E} C_i H e(t-d(t)) - e_k^T(t) \bar{E}^T \Omega \bar{E} e_k(t) \\ & \quad + (\tau(t) - \tau_m) \zeta^T(t) M_{ij} R_1^{-1} M_{ij}^T \zeta(t) + (\tau_M - \tau(t)) \zeta^T(t) N_{ij} R_1^{-1} N_{ij}^T \zeta(t) + d(t) \zeta^T(t) T_{ij} R_3^{-1} T_{ij}^T \zeta(t) \\ & \quad + (d_M - d(t)) \zeta^T(t) S_{ij} R_3^{-1} S_{ij}^T \zeta(t) \} \end{aligned} \tag{39}$$

By using well-known Schur complement and Lemma 2, from (24), one can easily see that

$$\mathbb{E}\{\mathcal{L}V(t)\} \leq \mathbb{E}\{\mathcal{L}[\gamma^2 w^T(t)w(t) - \tilde{z}^T(t)\tilde{z}(t)]\} \tag{40}$$

As is well known, the remaining part of the proof is similar to those in [5] and so omitted here for simplicity. The proof is complete.

Based on Theorem 1, we are in position to design a filter in the form of (3). The explicit expression of the parameters of the designed filter are given in the following theorem.  $\square$

**Theorem 2.** For given positive scalars  $\gamma, \tau_m, \tau_M, d_M, \varepsilon_1, \varepsilon_2, \varepsilon_3$  and  $\sigma$ , system (21) is exponentially stable in the mean square under the event trigger scheme (7) if there exist matrices  $P_1 > 0, \bar{P}_3 > 0, \bar{Q}_1, \bar{Q}_2, \bar{Q}_3, \bar{R}_1, \bar{R}_2, \bar{R}_3, \Omega > 0, \bar{A}_{fj}, \bar{B}_{fj}, \bar{C}_{fj}$ , and  $\bar{M}_{ij}, \bar{N}_{ij}, \bar{T}_{ij}, \bar{S}_{ij}$  with appropriate dimensions, such that the following LMIs hold:

$$\Sigma^{ij} + \Sigma^{ji} < 0, \quad i \leq j \in \mathcal{S} \tag{41}$$

$$P_1 - \bar{P}_3 > 0 \tag{42}$$

where

$$\begin{aligned} \Sigma^{ij} &= \begin{bmatrix} \Phi_{11}^{ij} & * & * & * \\ \Phi_{21}^{ij} & \Phi_{22}^{ij} & * & * \\ \Phi_{31}^{ij} & 0 & \Phi_{33}^{ij} & * \\ \Phi_{41}^{ij}(s) & 0 & 0 & \Phi_{44}^{ij} \end{bmatrix}, \quad (s = 1, 2, 3, 4) \\ \Phi_{11}^{ij} &= \begin{bmatrix} \bar{\Gamma}_{ij1} & * & * & * & * & * & * & * & * \\ \bar{R}_2 & \bar{\Gamma}_{ij2} & * & * & * & * & * & * & * \\ \tilde{\Upsilon}_{ij31} & \bar{M}_{ij3} - \bar{M}_{ij2}^T & \bar{\Gamma}_{ij3} & * & * & * & * & * & * \\ 0 & 0 & \bar{N}_{ij4} - \bar{N}_{ij3}^T & \bar{\Gamma}_{ij4} & * & * & * & * & * \\ \tilde{\Upsilon}_{ij51} + \bar{T}_{ij5} - \bar{T}_{ij1}^T & 0 & 0 & 0 & \bar{\Gamma}_{ij5} & * & * & * & * \\ 0 & 0 & 0 & 0 & S_{ij6} - S_{ij5}^T & \bar{\Gamma}_{ij6} & * & * & * \\ \tilde{\Upsilon}_{ij71} & 0 & 0 & 0 & 0 & 0 & -\bar{E}^T \Omega \bar{E} & * & * \\ \tilde{\Upsilon}_{ij81} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -\gamma^2 I \end{bmatrix} \\ \bar{\Gamma}_{ij1} &= \tilde{\Upsilon}_{ij1} + \tilde{\Upsilon}_{ij1}^T + \bar{Q}_1 + \bar{Q}_2 + \bar{Q}_3 - \bar{R}_2 + \bar{T}_{ij1} + \bar{T}_{ij1}^T, \quad \tilde{\Upsilon}_{ij1} = \begin{bmatrix} P_1 A_i & \bar{A}_{fj} \\ \bar{P}_3 A_i & \bar{A}_{fj} \end{bmatrix}, \\ \tilde{\Upsilon}_{ij31} &= \begin{bmatrix} A_{di}^T P_1 & A_{di}^T \bar{P}_3 \\ 0 & 0 \end{bmatrix}, \quad \bar{\Gamma}_{ij2} = -\bar{Q}_1 - \bar{R}_2 + \bar{M}_{ij2} + \bar{M}_{ij2}^T \\ \bar{\Gamma}_{ij3} &= -\bar{M}_{ij3} - \bar{M}_{ij3}^T + \bar{N}_{ij3} + \bar{N}_{ij3}^T, \quad \bar{\Gamma}_{ij4} = -\bar{Q}_2 - \bar{N}_{ij4} - \bar{N}_{ij4}^T \end{aligned}$$

$$\begin{aligned} \bar{\Gamma}_{ij5} &= \tilde{\Upsilon}_{ij5} - \bar{T}_{ij5} - \bar{T}_{ij5}^T + \bar{S}_{ij5} + \bar{S}_{ij5}^T, & \bar{\Gamma}_{ij6} &= -\bar{Q}_3 - \bar{S}_{ij6} - \bar{S}_{ij6}^T \\ \tilde{\Upsilon}_{ij51} &= \begin{bmatrix} C_i^T \bar{\Xi}^T \bar{B}_{fj}^T & C_i^T \bar{\Xi}^T \bar{B}_{fj}^T \\ 0 & 0 \end{bmatrix}, & \tilde{\Upsilon}_{ij5} &= \begin{bmatrix} \rho C_i^T \bar{\Xi}^T \Omega \bar{\Xi} C_i & 0 \\ 0 & 0 \end{bmatrix}, \\ \tilde{\Upsilon}_{ij71} &= [\bar{\Xi}^T \bar{B}_{fj}^T \quad \bar{\Xi}^T \bar{B}_{fj}^T], & \tilde{\Upsilon}_{ij81} &= [A_{wi}^T P_1 \quad A_{wi}^T \bar{P}_3] \\ \Omega_{21}^{ij} &= \begin{bmatrix} \tilde{L}_{ij} & 0_{p \times 2n} & 0_{p \times 2n} & 0_{p \times 2n} & 0_{p \times 2n} & 0_{p \times 2n} & 0_{p \times m} & 0_{p \times n} \\ \sqrt{\tau_{21}} \tilde{\Upsilon}_{ij1} & 0_{2n \times 2n} & \sqrt{\tau_{21}} \tilde{\Upsilon}_{ij31}^T & 0_{2n \times 2n} & \sqrt{\tau_{21}} \tilde{\Upsilon}_{ij51}^T & 0_{2n \times 2n} & \sqrt{\tau_{21}} \tilde{\Upsilon}_{ij71}^T & \sqrt{\tau_{21}} \tilde{\Upsilon}_{ij81}^T \\ \tau_m \tilde{\Upsilon}_{ij1} & 0_{2n \times 2n} & \tau_m \tilde{\Upsilon}_{ij31}^T & 0_{2n \times 2n} & \tau_m \tilde{\Upsilon}_{ij51}^T & 0_{2n \times 2n} & \tau_m \tilde{\Upsilon}_{ij71}^T & \tau_m \tilde{\Upsilon}_{ij81}^T \\ \sqrt{d_M} \tilde{\Upsilon}_{ij1} & 0_{2n \times 2n} & \sqrt{d_M} \tilde{\Upsilon}_{ij31}^T & 0_{2n \times 2n} & \sqrt{d_M} \tilde{\Upsilon}_{ij51}^T & 0_{2n \times 2n} & \sqrt{d_M} \tilde{\Upsilon}_{ij71}^T & \sqrt{d_M} \tilde{\Upsilon}_{ij81}^T \end{bmatrix} \\ \Phi_{22}^{ij} &= \text{diag}\{-I, -2\varepsilon_1 \bar{P} + \varepsilon_1^2 \bar{R}_1, -2\varepsilon_2 \bar{P} + \varepsilon_2^2 \bar{R}_2, -2\varepsilon_3 \bar{P} + \varepsilon_3^2 \bar{R}_3\}, & \bar{P} &= \begin{bmatrix} P_1 & \bar{P}_3 \\ \bar{P}_3 & \bar{P}_3 \end{bmatrix} \end{aligned}$$

$$\mathfrak{R}_k = \text{diag}\{\underbrace{-2\varepsilon_k \bar{P} + \varepsilon_k^2 \bar{R}_k, \dots, -2\varepsilon_k \bar{P} + \varepsilon_k^2 \bar{R}_k}_m\}, \quad k = 1, 2, 3.$$

$$\begin{aligned} \Phi_{33}^{ij} &= \text{diag}\{\mathfrak{R}_1, \mathfrak{R}_2, \mathfrak{R}_3\}, & \Omega_{44}^{ij} &= \text{diag}\{-\bar{R}_1, -\bar{R}_3\}, & \tilde{L}_{ij} &= [L_i \quad -\bar{C}_{fj}] \\ \Omega_{31}^{ij} &= \begin{bmatrix} 0_{2n \times 2n} & 0_{2n \times 2n} & 0_{2n \times 2n} & 0_{2n \times 2n} & \check{D}_{12} & 0_{2n \times 2n} & 0_{2n \times m} & 0_{2n \times n} \\ 0_{2n \times 2n} & 0_{2n \times 2n} & 0_{2n \times 2n} & 0_{2n \times 2n} & \check{D}_{22} & 0_{2n \times 2n} & 0_{2n \times m} & 0_{2n \times n} \\ 0_{2n \times 2n} & 0_{2n \times 2n} & 0_{2n \times 2n} & 0_{2n \times 2n} & \check{D}_{32} & 0_{2n \times 2n} & 0_{2n \times m} & 0_{2n \times n} \end{bmatrix}, & \check{D}_{12} &= \begin{bmatrix} \sqrt{\tau_{21}} \delta_1 \hat{D}_{12} \\ \vdots \\ \sqrt{\tau_{21}} \delta_m \hat{D}_{m2} \end{bmatrix} \\ \check{D}_{22} &= \begin{bmatrix} \delta_1 \tau_m \hat{D}_{12} \\ \vdots \\ \delta_1 \tau_m \delta_m \hat{D}_{m2} \end{bmatrix}, & \check{D}_{32} &= \begin{bmatrix} \sqrt{d_M} \delta_1 \hat{D}_{12} \\ \vdots \\ \sqrt{d_M} \delta_m \hat{D}_{m2} \end{bmatrix}, & \hat{D}_{l2} &= \begin{bmatrix} \bar{B}_{fj} E_l C_i & 0 \\ \bar{B}_{fj} E_l C_i & 0 \end{bmatrix}, \quad l = 1, 2, \dots, m \\ \Phi_{41}^{ij}(1) &= \begin{bmatrix} \sqrt{\tau_{21}} \bar{M}_{ij}^T \\ \sqrt{d_M} \bar{T}_{ij}^T \end{bmatrix}, & \Phi_{41}^{ij}(2) &= \begin{bmatrix} \sqrt{\tau_{21}} \bar{M}_{ij}^T \\ \sqrt{d_M} \bar{S}_{ij}^T \end{bmatrix}, & \Phi_{41}^{ij}(3) &= \begin{bmatrix} \sqrt{\tau_{21}} \bar{N}_{ij}^T \\ \sqrt{d_M} \bar{S}_{ij}^T \end{bmatrix}, & \Phi_{41}^{ij}(4) &= \begin{bmatrix} \sqrt{\tau_{21}} \bar{N}_{ij}^T \\ \sqrt{d_M} \bar{T}_{ij}^T \end{bmatrix} \\ \bar{M}_{ij}^T &= [0_{2n \times 2n} \quad \bar{M}_{ij2}^T \quad \bar{M}_{ij3}^T \quad 0_{2n \times 2n} \quad 0_{2n \times 2n} \quad 0_{2n \times 2n} \quad 0_{2n \times m} \quad 0_{2n \times n}] \\ \bar{N}_{ij}^T &= [0_{2n \times 2n} \quad 0_{2n \times 2n} \quad \bar{N}_{ij3}^T \quad \bar{N}_{ij4}^T \quad 0_{2n \times 2n} \quad 0_{2n \times 2n} \quad 0_{2n \times m} \quad 0_{2n \times n}] \\ \bar{T}_{ij}^T &= [\bar{T}_{ij1}^T \quad 0_{2n \times 2n} \quad 0_{2n \times 2n} \quad 0_{2n \times 2n} \quad \bar{T}_{ij5}^T \quad 0_{2n \times 2n} \quad 0_{2n \times m} \quad 0_{2n \times n}] \\ \bar{S}_{ij}^T &= [0_{2n \times 2n} \quad 0_{2n \times 2n} \quad 0_{2n \times 2n} \quad 0_{2n \times 2n} \quad \bar{S}_{ij5}^T \quad \bar{S}_{ij6}^T \quad 0_{2n \times m} \quad 0_{2n \times n}] \end{aligned}$$

Moreover, if the above conditions are feasible, the parameter matrices of the filter are given by

$$\begin{cases} A_{fj} = \bar{A}_{fj} \bar{P}_3^{-1} \\ B_{fj} = \bar{B}_{fj} \\ C_{fj} = \bar{C}_{fj} \bar{P}_3^{-1}, \end{cases} \quad j \in \mathbb{S} \tag{43}$$

**Proof.** Due to

$$(R_k - \varepsilon_k^{-1} P) R_k^{-1} (R_k - \varepsilon_k^{-1} P) \geq 0, \quad (k = 1, 2, 3)$$

we have

$$-P R_k^{-1} P \leq -2\varepsilon_k P + \varepsilon_k^2 R_k$$

Substitute  $-P R_k^{-1} P$  with  $-2\varepsilon_k P + \varepsilon_k^2 R_k$  ( $k = 1, 2, 3$ ) into (41), we can obtain

$$\Pi^{ij} + \Pi^{ji} > 0 \tag{44}$$

where

$$\begin{aligned} \bar{\Pi}^{ij} &= \begin{bmatrix} \Omega_{11}^{ij} + \Upsilon + \Upsilon^T & * & * & * \\ \Omega_{21}^{ij} & \bar{\Omega}_{22}^{ij} & * & * \\ \Omega_{31}^{ij} & 0 & \bar{\Omega}_{33}^{ij} & * \\ \Omega_{41}^{ij}(s) & 0 & 0 & \Omega_{44}^{ij} \end{bmatrix}, \quad (s = 1, 2, 3, 4), \\ \bar{\Omega}_{22}^{ij} &= \text{diag}\{-I, -2\varepsilon_1 P + \varepsilon_1^2 R_1, -2\varepsilon_2 P + \varepsilon_2^2 R_2, -2\varepsilon_3 P + \varepsilon_3^2 R_3\}, \\ \bar{\Omega}_{33}^{ij} &= \text{diag}\{\bar{\mathfrak{R}}_1, \bar{\mathfrak{R}}_2, \bar{\mathfrak{R}}_3\}, \\ \bar{\mathfrak{R}}_k &= \text{diag}\{\underbrace{-2\varepsilon_k P + \varepsilon_k^2 R_k, \dots, -2\varepsilon_k P + \varepsilon_k^2 R_k}_m\}, \quad k = 1, 2, 3. \end{aligned}$$

Since  $\bar{P}_3 > 0$ , there exist  $P_2$  and  $P_3 > 0$  satisfying  $\bar{P}_3 = P_2^T P_3^{-1} P_2$ .

Define

$$P = \begin{bmatrix} P_1 & P_2^T \\ P_2 & P_3 \end{bmatrix}, \quad J = \begin{bmatrix} I & 0 \\ 0 & P_2^T P_3^{-1} \end{bmatrix}, \quad F = \text{diag}\{\underbrace{J, \dots, J}_6, I, I, I, \underbrace{J, \dots, J}_{3m+5}\} \tag{45}$$

By Schur complement,  $P > 0$  is equivalent to  $P_1 - \bar{P}_3 > 0$ .

Multiply (44) by  $F$  from the left side and its transpose from the right side, respectively, and defining  $\bar{P} = J P J^T = \begin{bmatrix} P_1 & P_2^T \\ P_2 & P_3 \end{bmatrix}$ ,  $\bar{Q}_k = J Q_k J^T$ ,  $\bar{R}_k = J R_k J^T$  ( $k = 1, 2, 3$ ),  $\bar{M}_{ijv_1} = J M_{ijv_1} J^T$ ,  $\bar{N}_{ijv_2} = J N_{ijv_2} J^T$ ,  $\bar{T}_{ijv_3} = J T_{ijv_3} J^T$ ,  $\bar{S}_{ijv_4} = J S_{ijv_4} J^T$ , ( $v_1 = 2, 3$ ;  $v_2 = 3, 4$ ;  $v_3 = 1, 5$ ;  $v_4 = 5, 6$ ). Define variables

$$\begin{cases} \bar{A}_{fj} = \hat{A}_{fj} \bar{P}_3, \hat{A}_{fj} = P_2^T A_{fj} P_2^{-T} \\ \bar{B}_{fj} = P_2^T B_{fj} \\ \bar{C}_{fj} = \hat{C}_{fj} \bar{P}_3, \hat{C}_{fj} = C_{fj} P_2^{-T} \end{cases} \tag{46}$$

Then, (24) is equivalent to (41) for  $s = 1, 2, 3, 4$ , respectively.

Next, we will show that, if (41) are solvable for  $\bar{A}_{fj}$ ,  $\bar{B}_{fj}$ ,  $\bar{C}_{fj}$  and  $\bar{P}_3$ , then the parameter matrices of the filter (4) can be chosen as in (43).

Replacing the filter parameters  $(A_{fj}, B_{fj}, C_{fj})$  by  $(P_2^{-T} \hat{A}_{fj} P_2^T, P_2^{-T} \bar{B}_{fj}, \hat{C}_{fj} P_2^T)$ , in (4), then, the filter (4) can be rewritten as

$$\begin{cases} \dot{x}_f(t) = P_2^{-T} \hat{A}_{fj} P_2^T x_f(t) + P_2^{-T} \bar{B}_{fj} \hat{y}(t) \\ z_f(t) = \hat{C}_{fj} P_2^T x_f(t) \end{cases} \tag{47}$$

Defining  $\hat{x}(t) = P_2^T x_f(t)$ , similar to the analysis of [20], (47) becomes

$$\begin{cases} \dot{\hat{x}}(t) = \hat{A}_{fj} \hat{x}(t) + \bar{B}_{fj} \hat{y}(t) \\ z_f(t) = \hat{C}_{fj} \hat{x}(t) \end{cases} \tag{48}$$

That is  $(\hat{A}_{fj}, \hat{B}_{fj}, \hat{C}_{fj})$  can be chosen as the filter parameters.

Then, from (46) and (48), we can obtain that the parameter matrices of the filter are given by (43). This completes the proof.  $\square$

**Remark 10.** The introduction of event-triggered scheme (7), which can reduce the communication load, is an effective way to deal with the issue of limited resource and insufficient communication bandwidth and the case of inadequate computation power. Under the event-triggered mechanism (7), taking the probabilistic sensor failure into consideration, we provides a new filter design method in Theorem 2, which is expected to obtain better performance.

#### 4. Simulation examples

Consider a specific T–S fuzzy system of Eq. (2) under a network control system structure, in which the system parameters are given as follows:

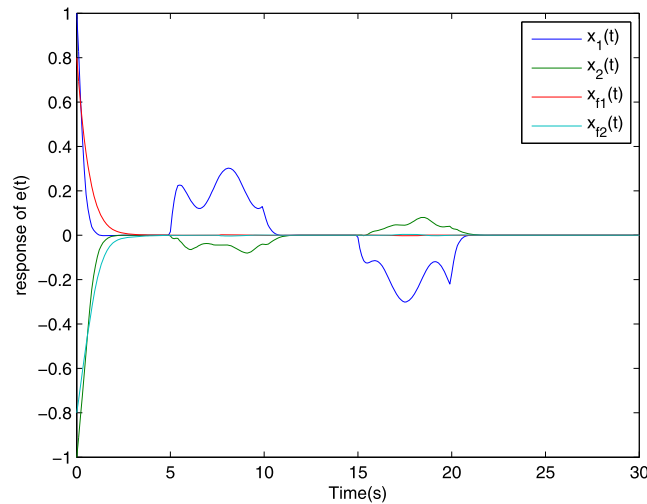


Fig. 2. Responses of  $e(t)$  in Case 1.

$$\begin{aligned}
 A_1 &= \begin{bmatrix} -2.1 & 0.1 \\ 1 & -2 \end{bmatrix}, & A_2 &= \begin{bmatrix} -1.9 & 0 \\ -0.2 & -1.1 \end{bmatrix}, & A_{d1} &= \begin{bmatrix} -1.1 & 0.1 \\ -0.8 & -0.9 \end{bmatrix} \\
 A_{d2} &= \begin{bmatrix} -0.9 & 0 \\ -1.1 & -1.2 \end{bmatrix}, & A_{w1} &= \begin{bmatrix} 1 \\ -0.2 \end{bmatrix}, & A_{w2} &= \begin{bmatrix} 0.3 \\ 0.1 \end{bmatrix}, & C_1 &= [1 \quad 0] \\
 C_2 &= [0.5 \quad -0.6], & L_1 &= [1 \quad -0.5], & L_2 &= [-0.2 \quad 0.3] \\
 h_1(\theta(t)) &= \sin^2 t, & h_2(\theta(t)) &= \cos^2 t \\
 w(t) &= \begin{cases} 1 & 5 \leq t \leq 10 \\ -1 & 15 \leq t \leq 20 \\ 0 & \text{else} \end{cases}
 \end{aligned}$$

In the following, we will consider three possible cases, which can show the effectiveness of the event-triggered scheme and the effect of the sensor failure rate on the system performance.

*Case 1:* when the sensors are in good condition, that is  $\mathcal{E} = I$ , we assume  $\tau_m = 0.1$ ,  $\tau_M = 0.3$ ,  $d_M = 0.6$ ,  $\gamma = 1.2$  and the corresponding trigger parameter  $\rho = 0.9$ , by using the LMI toolbox of Matlab, we can obtain the corresponding trigger matrix  $\Omega = 0.1234$  and the following matrices:

$$\begin{aligned}
 P_1 &= \begin{bmatrix} 2.0292 & -0.0247 \\ -0.0247 & 2.0478 \end{bmatrix}, & \bar{P}_3 &= \begin{bmatrix} 0.6623 & -0.0203 \\ -0.0203 & 0.9285 \end{bmatrix} \\
 \bar{A}_{f1} &= \begin{bmatrix} -1.2972 & 0.0323 \\ 0.8823 & -1.2050 \end{bmatrix}, & \bar{B}_{f1} &= \begin{bmatrix} 0.0352 \\ -0.0557 \end{bmatrix}, & \bar{C}_{f1} &= [-0.5689 \quad 0.4166] \\
 \bar{A}_{f2} &= \begin{bmatrix} -0.7089 & 0.3509 \\ -0.3065 & -1.1306 \end{bmatrix}, & \bar{B}_{f2} &= \begin{bmatrix} -0.0255 \\ 0.0403 \end{bmatrix}, & \bar{C}_{f2} &= [0.2071 \quad -0.1213]
 \end{aligned}$$

Then, by using [Theorem 2](#), we can get the filter parameters as follows:

$$\begin{aligned}
 A_{f1} &= \begin{bmatrix} -1.9588 & -0.0081 \\ 1.2932 & -1.2695 \end{bmatrix}, & B_{f1} &= \begin{bmatrix} 0.0352 \\ -0.0557 \end{bmatrix}, & C_{f1} &= [-0.8458 \quad 0.4302] \\
 A_{f2} &= \begin{bmatrix} -1.0595 & 0.3548 \\ -0.5005 & -1.2287 \end{bmatrix}, & B_{f2} &= \begin{bmatrix} -0.0255 \\ 0.0403 \end{bmatrix}, & C_{f2} &= [0.3089 \quad -0.1238]
 \end{aligned}$$

For the initial condition  $x(0) = [1 \quad -1]^T$ ,  $x_f(0) = [0.8 \quad -0.8]^T$  and the sampling period  $h = 0.1$ , the simulation result for the responses of  $e(t)$  is shown in [Fig. 2](#). From the simulation, it can be found that with the use of the proposed method, the designed filter can satisfy the system performance.

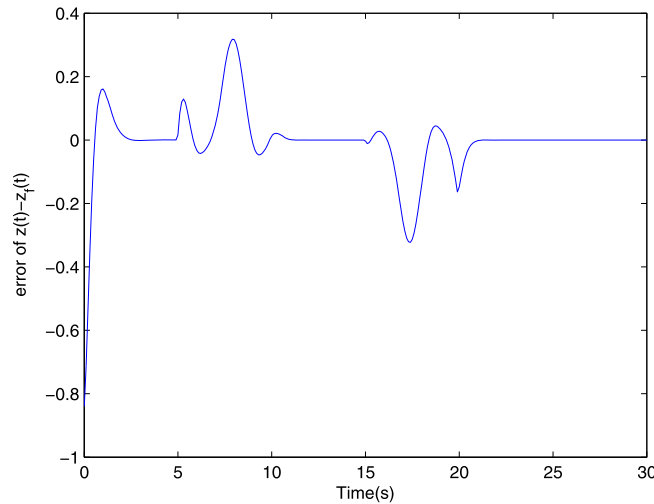


Fig. 3. Responses of  $\tilde{z}(t)$  in Case 2.

Case 2: The parameters for the sensor failure are  $\bar{\mathcal{E}} = 0.8$  and  $\delta = 0.05$ . When corresponding triggered parameter  $\rho = 0$ , the system reduces to time triggered. Set  $\tau_m = 0.1$ ,  $\tau_M = 0.3$ ,  $d_M = 0.6$ ,  $\gamma = 1.2$ , we can get the corresponding trigger matrix  $\Omega = 28.6111$  and the following matrices:

$$P_1 = \begin{bmatrix} 2.0687 & 0.0028 \\ 0.0028 & 2.2237 \end{bmatrix}, \quad \bar{P}_3 = \begin{bmatrix} 0.6769 & -0.0171 \\ -0.0171 & 1.0270 \end{bmatrix}$$

$$\bar{A}_{f1} = \begin{bmatrix} -1.3167 & 0.0405 \\ 0.9658 & -1.3387 \end{bmatrix}, \quad \bar{B}_{f1} = \begin{bmatrix} 0.0972 \\ -0.1796 \end{bmatrix}, \quad \bar{C}_{f1} = [-0.5666 \quad 0.4389]$$

$$\bar{A}_{f2} = \begin{bmatrix} -0.7405 & 0.3841 \\ -0.3176 & -1.2814 \end{bmatrix}, \quad \bar{B}_{f2} = \begin{bmatrix} -0.1493 \\ 0.2756 \end{bmatrix}, \quad \bar{C}_{f2} = [0.2105 \quad -0.1261]$$

With the application of the filter design method developed in Theorem 2, the filter parameters are obtained as

$$A_{f1} = \begin{bmatrix} -1.9451 & 0.0070 \\ 1.3944 & -1.2803 \end{bmatrix}, \quad B_{f1} = \begin{bmatrix} 0.0972 \\ -0.1796 \end{bmatrix}, \quad C_{f1} = [-0.8266 \quad 0.4136]$$

$$A_{f2} = \begin{bmatrix} -1.0849 & 0.3559 \\ -0.5010 & -1.2561 \end{bmatrix}, \quad B_{f2} = \begin{bmatrix} -0.1493 \\ 0.2756 \end{bmatrix}, \quad C_{f2} = [0.3080 \quad -0.1176]$$

For the initial condition  $x(0) = [1 \quad -1]^T$ ,  $x_f(0) = [0.8 \quad -0.8]^T$  and the sampling period  $h = 0.1$ , the response of filter error  $\tilde{z}(t)$  is depicted in Fig. 3. The probabilistic sensor faults are shown in Fig. 4. It is seen from the simulation that with the sensor fault appearance, the designed filter can also satisfy the system performance.

Case 3: when the system is under the event-triggered scheme, let the corresponding trigger parameter  $\rho = 0.9$  and  $\bar{\mathcal{E}} = 0.8$ ,  $\delta = 0.05$ ,  $\tau_m = 0.1$ ,  $\tau_M = 0.3$ ,  $d_M = 0.6$ ,  $\gamma = 1.2$ , by applying Theorem 2, we can obtain the corresponding trigger matrix  $\Omega = 0.1926$  and the following matrices:

$$P_1 = \begin{bmatrix} 2.0293 & -0.0247 \\ -0.0247 & 2.0481 \end{bmatrix}, \quad \bar{P}_3 = \begin{bmatrix} 0.6624 & -0.0203 \\ -0.0203 & 0.9286 \end{bmatrix}$$

$$\bar{A}_{f1} = \begin{bmatrix} -1.2974 & 0.0323 \\ 0.8826 & -1.2052 \end{bmatrix}, \quad \bar{B}_{f1} = \begin{bmatrix} 0.0440 \\ -0.0695 \end{bmatrix}, \quad \bar{C}_{f1} = [-0.5689 \quad 0.4167]$$

$$\bar{A}_{f2} = \begin{bmatrix} -0.7090 & 0.3510 \\ -0.3066 & -1.1308 \end{bmatrix}, \quad \bar{B}_{f2} = \begin{bmatrix} -0.0319 \\ 0.0503 \end{bmatrix}, \quad \bar{C}_{f2} = [0.2071 \quad -0.1213]$$

Then, by applying Theorem 2, the filter parameters are derived as follows:

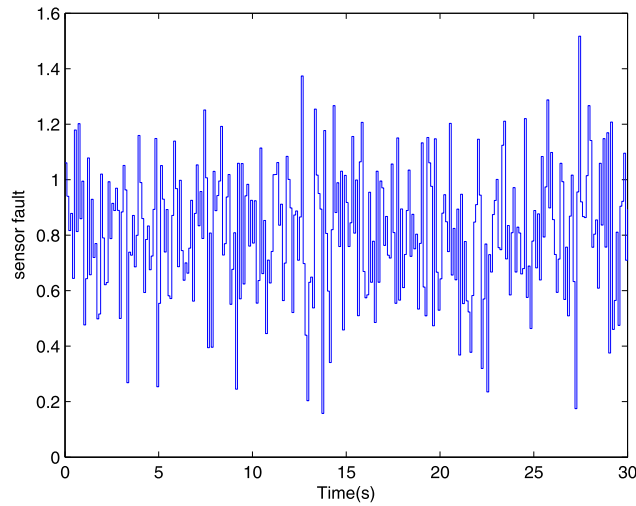


Fig. 4. The probabilistic sensor fault in Case 2.

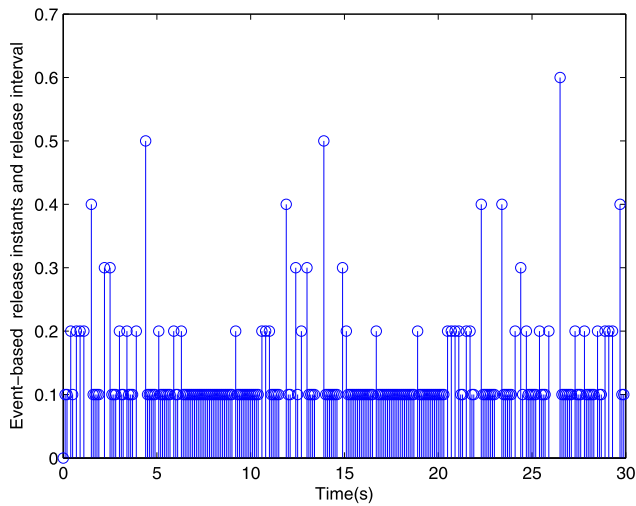


Fig. 5. The release instants and the release interval in Case 3.

$$\begin{aligned}
 A_{f1} &= \begin{bmatrix} -1.9589 & -0.0081 \\ 1.2934 & -1.2695 \end{bmatrix}, & B_{f1} &= \begin{bmatrix} 0.0440 \\ -0.0695 \end{bmatrix}, & C_{f1} &= [-0.8457 \quad 0.4302] \\
 A_{f2} &= \begin{bmatrix} -1.0594 & 0.3548 \\ -0.5006 & -1.2287 \end{bmatrix}, & B_{f2} &= \begin{bmatrix} -0.0319 \\ 0.0503 \end{bmatrix}, & C_{f2} &= [0.3089 \quad -0.1238]
 \end{aligned}$$

For the initial condition  $x(0) = [1 \quad -1]^T$ ,  $x_f(0) = [0.8 \quad -0.8]^T$  and the sampling period  $h = 0.1$ , the event-triggering release instants and intervals are shown in Fig. 5. The simulation result for the responses of  $e(t)$  are shown in Fig. 6, which demonstrate that the designed filter can satisfy the system performance.

### 5. Conclusion

The reliable  $H_\infty$  filter design for an event-based network control systems via T–S fuzzy model has been investigated. In particular, the event-triggered scheme inserted in the network has the advantages of reducing the communication load in the network and gearing up its efficiency. Moreover, employing the networked T–S fuzzy model with probabilistic sensor faults and the event triggered scheme, the fundamental stability criteria are obtained,

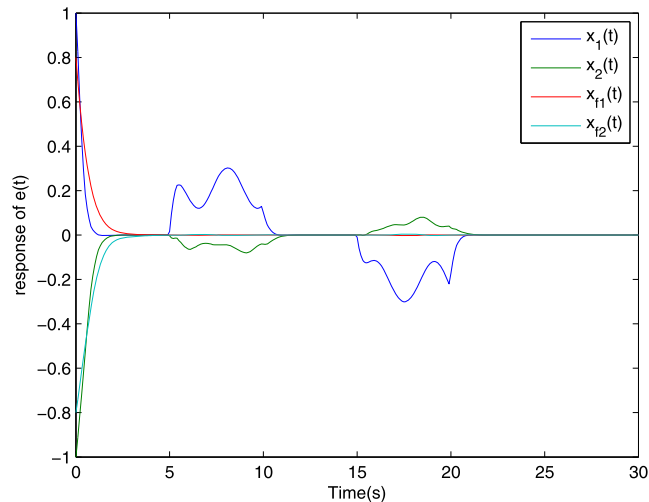


Fig. 6. Responses of  $e(t)$  in Case 3.

and a filter design method is developed. Then the explicit expression of the desired filter parameters has been derived. Lastly, a numerical example has been provided to show the usefulness and effectiveness of the proposed method.

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